

# Experimental validation of a nonequilibrium model of CO<sub>2</sub> fluxes between gas, liquid medium, and algae in a flat-panel photobioreactor

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**Abstract** Carbon dioxide (CO<sub>2</sub>) availability strongly affects the productivity of algal photobioreactors, where it is dynamically exchanged between different compartments, phases, and chemical forms. To understand the underlying processes, we constructed a nonequilibrium mathematical model of CO<sub>2</sub> dynamics in a flat-panel algal photobioreactor. The model includes mass transfer to the algal suspension from a stream of bubbles of CO<sub>2</sub>-enriched air and from the photobioreactor headspace. Also included are the hydration of dissolved CO<sub>2</sub> to bicarbonate ion (HCO<sub>3</sub><sup>-</sup>) as well as uptake and/or cycling of these two chemical forms by the cells. The model was validated in experiments using a laboratory-scale flat-panel photobioreactor that controls light, temperature, and pH and where the concentration of dissolved CO<sub>2</sub>, and partial pressure of CO<sub>2</sub> in the photobioreactor exhaust are measured. First, the model prediction was compared with measured CO<sub>2</sub> dynamics that occurred in response to a stepwise change in the CO<sub>2</sub> partial pressure in the gas sparger. Furthermore, the model was used to predict CO<sub>2</sub> dynamics in photobioreactors with unicellular, nitrogen-fixing cyanobacterium *Cyanothece* sp. The metabolism changes dramatically during a day, and the distribution of CO<sub>2</sub> is expected to exhibit a pronounced

diurnal modulation that significantly deviates from chemical equilibrium.

**Keywords** Algae · Carbon dioxide · Cyanobacteria · Mathematical model · Photosynthesis

## List of symbols

$a_B$	Specific gas–liquid interfacial bubble area (m <sup>-1</sup> )
$h$	Henry constant (m <sup>3</sup> Pa mol <sup>-1</sup> )
$k$	Rate of CO <sub>2</sub> hydration (s <sup>-1</sup> )
$k_L$	Liquid-phase mass transfer coefficient (m s <sup>-1</sup> )
$l$	Rate of HCO <sub>3</sub> <sup>-</sup> dehydration (s <sup>-1</sup> )
$n_{CO_2}$	Number of CO <sub>2</sub> molecules (mol)
$r_B$	Bubble radius (m)
$J$	Aeration rate (m <sup>3</sup> s <sup>-1</sup> )
$N_B$	Number of bubbles
$p_{CO_2}^{bubble}$	Partial CO <sub>2</sub> pressure inside bubble (Pa)
$p_{CO_2}^{IN}$	Partial CO <sub>2</sub> pressure of gas entering bioreactor (Pa)
$p_{CO_2}^{OUT}$	Partial CO <sub>2</sub> pressure of gas leaving bioreactor headspace (Pa)
$p_{CO_2}^X$	Partial CO <sub>2</sub> pressure of bubble entering bioreactor headspace (Pa)
$R$	Universal gas constant (m <sup>3</sup> Pa K <sup>-1</sup> mol <sup>-1</sup> )
$S_B$	Bubble surface (m <sup>2</sup> )
$S_H$	Liquid to headspace surface (m <sup>2</sup> )
$T$	Temperature of the photobioreactor (K)
$V_B$	Volume of bubble (m <sup>3</sup> )
$V_H$	Volume of headspace (m <sup>3</sup> )
$V_L$	Volume of liquid (m <sup>3</sup> )
$\alpha_{CO_2}$	Mass transfer rate from bubble to liquid phase (mol s <sup>-1</sup> )
$\beta_{CO_2}$	Mass transfer rate from headspace to liquid phase (mol s <sup>-1</sup> )

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$\gamma_{\text{dCO}_2}$	Rate of dissolved carbon dioxide uptake by algae ( $\text{mol s}^{-1}$ )
$\gamma_{\text{HCO}_3^-}$	Rate of bicarbonate uptake by algae ( $\text{mol s}^{-1}$ )
$\tau$	Bubble lifetime (s)
$A$	Flux of $\text{CO}_2$ into bioreactor ( $\text{mol s}^{-1}$ )
$B$	Flux of $\text{CO}_2$ into headspace ( $\text{mol s}^{-1}$ )
$\Gamma$	Flux of $\text{CO}_2$ out of bioreactor ( $\text{mol s}^{-1}$ )
$[\text{dCO}_2]$	Concentration of $\text{CO}_2$ dissolved in liquid phase ( $\text{mol m}^{-3}$ )
$[\text{HCO}_3^-]$	Concentration of bicarbonate ions in liquid phase ( $\text{mol m}^{-3}$ )

## Introduction

It is of immense importance to develop carbon-neutral or even carbon-capturing technologies that may mitigate the dynamics of the climatic implications of rising anthropogenic  $\text{CO}_2$  emissions [6]. To operate on the scale of natural carbon cycle pools [11], one has to consider processes of proportional capacity such as photosynthesis, which has played the decisive role in stabilizing the global ecosystem within the present limits for billions of years [12]. Today, photosynthesis also promises production of third-generation biofuels that may assist in recycling atmospheric  $\text{CO}_2$  [1, 4]. Photosynthetic microorganisms are also considered for biomineralization by point-source carbon capture [8, 20]. In another representation of biological carbon capture,  $\text{CO}_2$  is an important substrate for intensive culturing of microalgae [5, 18].  $\text{CO}_2$ -enriched air used for sparging was shown to enhance the productivity of microalgae under both laboratory and industrial mass culture conditions [1, 25, 30].

Among the processes that need to be better understood is the mass transfer of  $\text{CO}_2$  between the gaseous and liquid phases of algal culture systems as well as the dynamics of dissolved inorganic carbon (Ci) that is, typically, in the form of aqueous dissolved  $\text{CO}_2$  ( $\text{dCO}_2$ ) or bicarbonate ion ( $\text{HCO}_3^-$ ). The capacity of the particular organism to utilize preferably either  $\text{dCO}_2$  or  $\text{HCO}_3^-$  is species dependent [7, 9, 19]. Furthermore, massive biological cycling of Ci has been demonstrated in representatives of the main algal groups [27]. Some algae take up  $\text{CO}_2$  from the medium and release  $\text{HCO}_3^-$ , whereas others transport  $\text{HCO}_3^-$  inward and release excess  $\text{CO}_2$ . In some cases, the cycling may reach values 7 times larger than the rate of net photosynthesis [26]. Cycling of Ci constitutes part of the  $\text{CO}_2$  concentrating mechanism [7, 9, 16] shown to raise the  $\text{CO}_2$  concentration in close proximity to the universal carboxylating enzyme, ribulose 1,5-bisphosphate carboxylase/oxygenase (Rubisco) in most algal systems examined to date [19].

Thus, one needs to understand the entire system from gas sparging in the algal units to biological assimilation and cycling. To address these challenges, we developed and herein present a mathematical model of  $\text{CO}_2$  mass transfer dynamics in a flat-panel algal photobioreactor [2, 15]. Model parameters allow simulation of different scenarios that may be relevant in industrial applications. The model is validated in a set of technical and biological experiments.

## Materials and methods

### Culture conditions

The unicellular nitrogen-fixing cyanobacterium *Cyanot- hece* sp. ATCC 51142 [13, 21, 23] was cultured in artificial ASP2 seawater medium [17] as modified [29] without nitrate. The pH of the medium was buffered at pH 7.5 using 17 mM TAPS biological buffer, and temperature was stabilized at  $30 \pm 0.2^\circ\text{C}$ . For a detailed description of experimental protocols see [3].

### Photobioreactor

The growth chamber of the temperature-controlled bioreactor unit (FMT-150, Photon Systems Instruments, Brno, Czech Republic) consists of a parallel-plate glass cuvette ( $20 \text{ cm} \times 10.1 \text{ cm} \times 6 \text{ cm}$ ) filled with 1,200 ml liquid media or algal suspension depending on experiment setup (see “[Liquid media for the technical experiments](#)” section for more details). The capabilities of the bioreactor were expanded by including gas-mixing and gas-analyzing utilities, and by incorporation of electrodes for measuring levels of  $\text{CO}_2$  and  $\text{O}_2$  dissolved in the suspension [2]. Specific gas mixture was dispersed into seven bubble streams by orifices in a stainless-steel tube at the bottom of the bioreactor cuvette. Other construction details of the instrument have been described previously [15].

### Gas composition and flow rate control

A mass flow control system (GMS-150; Photon Systems Instruments, Brno, Czech Republic), was used to stabilize the composition of the  $\text{CO}_2$ -enriched gas supply. The gas flow through the photobioreactor was measured by MASS-VIEW (Bronkhorst High-Tech BV, Ruurlo, The Netherlands) and controlled by a high-precision valve (Parker Hannifin, Cleveland, USA). The composition of the exhaust gas escaping from the photobioreactor was monitored by an infrared  $\text{CO}_2$  gas analyzer (Vaisala, Helsinki, Finland).

Liquid media for the technical experiments

The model was validated using media of pH 4.0 and pH 7.4, in which the CO<sub>2</sub> appears dominantly as dCO<sub>2</sub> and HCO<sub>3</sub><sup>-</sup>, respectively. The pH 4.0 medium was prepared from deionized H<sub>2</sub>O by adding 30 ml acetic buffer solution (0.1 M acetic acid, 0.02 M NaOH, adjusted to pH 4.0). The pH 7.4 medium was prepared by using TAPS biological buffer (17 mM, [(2-hydroxy-1,1-bis(hydroxymethyl)ethyl) amino]-1-propanesulfonic acid; Sigma, St. Louis, USA). Long-term pH stability was continuously monitored during the experiments and maintained by drops of 0.2 M NaOH when needed.

Results and discussion

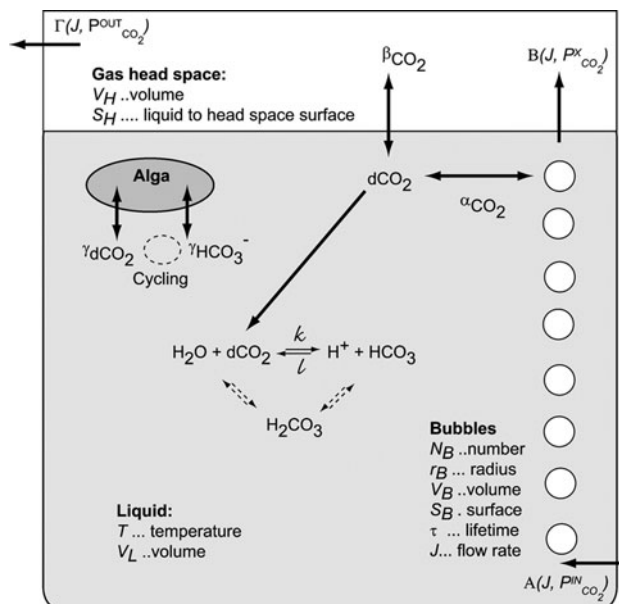
Model

The scheme in Fig. 1 shows the model compartments, components, and parameters. For simplicity, we assume that both the liquid and the gaseous headspace are perfectly mixed, leading to uniform molar concentrations and partial pressures within the respective compartments. The CO<sub>2</sub> partial pressure in a bubble of CO<sub>2</sub>-enriched air is high at the bottom of the photobioreactor and gradually decreases by mass transfer to the liquid while the bubble travels upward. The dynamics of the CO<sub>2</sub> partial pressure inside the bubble is described by  $P_{CO_2(t)}^{bubble}$ , where  $t$  is the time between the bubble leaving the sparging tube at  $t = 0$  s ( $P_{CO_2(t=0s)}^{bubble} = P_{CO_2}^{IN}$ ) and  $t = \tau$  s when emerging into the headspace ( $P_{CO_2(t=\tau)}^{bubble} \approx P_{CO_2}^X$ ). Using Henry’s law, the mass transfer rate between the bubble and the liquid phase can be calculated using Eq. (1):

$$\frac{\Delta n_{CO_2}}{\Delta t} = k_L S_B \left( \frac{P_{CO_2(t)}^{bubble}}{h} - [dCO_2]_{(t)} \right), \tag{1}$$

where  $k_L$  is the mass transfer coefficient,  $S_B$  is the surface of the bubble ( $\sim 4\pi r_B^2$ , where  $r_B$  is the effective bubble radius),  $P_{CO_2(t)}^{bubble}$  is the instantaneous CO<sub>2</sub> partial pressure in a bubble at time  $t$ ,  $h$  is the Henry constant at temperature  $T$ , and  $[dCO_2]$  is the concentration of CO<sub>2</sub> dissolved in the liquid phase. The mass transfer is, at the same time, changing the CO<sub>2</sub> partial pressure in the bubble:

$$\frac{\Delta n_{CO_2}}{\Delta t} = -\frac{V_B}{RT} \frac{dP_{CO_2(t)}^{bubble}}{dt}, \tag{2}$$



**Fig. 1** Scheme of CO<sub>2</sub> mass transfer in a flat-panel algal photobioreactor. CO<sub>2</sub>-enriched air enters the photobioreactor through a sparging tube, generating on average  $N_B$  bubbles of effective mean radius  $r_B$  (m). The average bubble lifetime is  $\tau$  (s). The gaseous and liquid phases are assumed to be of the same temperature  $T$  (K). The volume of the liquid phase is  $V_L$  (m<sup>3</sup>), and the surface between the liquid and the gaseous headspace is  $S_H$  (m<sup>2</sup>). The headspace volume is  $V_H$  (m<sup>3</sup>). The gas flow through the photobioreactor is constant at  $J$  (m<sup>3</sup> s<sup>-1</sup>), entering with CO<sub>2</sub> partial pressure of  $P_{CO_2}^{IN}$  (Pa), so that the resulting CO<sub>2</sub> mass transfer flux into the photobioreactor is  $A$  (mol s<sup>-1</sup>). The CO<sub>2</sub> partial pressure of the gas flow from bubbles to the headspace is  $P_{CO_2}^X$  (Pa), resulting in CO<sub>2</sub> flux of  $B$  (mol s<sup>-1</sup>). The CO<sub>2</sub> partial pressure in the headspace and in the exhaust gas is assumed to be uniform  $P_{CO_2}^{OUT}$  (Pa), leading to residual CO<sub>2</sub> flux out of the photobioreactor of  $\Gamma$  (mol s<sup>-1</sup>). The integral mass transfer flux of CO<sub>2</sub> from bubbles to the liquid medium is  $\alpha_{CO_2}$  (mol s<sup>-1</sup>), from the headspace to the liquid medium it is  $\beta_{CO_2}$  (mol s<sup>-1</sup>), from the pool of dissolved CO<sub>2</sub> to the algae it is  $\gamma_{dCO_2}$  (mol s<sup>-1</sup>), and from the bicarbonate pool to the algae  $\gamma_{HCO_3^-}$  (mol s<sup>-1</sup>). The two latter rate constants,  $\gamma_{dCO_2}$  and  $\gamma_{HCO_3^-}$ , reflect also the extracellular biological cycling between the two forms. A more technical description and drawing of the photobioreactor have been published previously [15]

where  $V_B$  is the effective volume of the bubble ( $\sim 4\pi r_B^2/3$ ) and  $R$  is the universal gas constant. The Eqs. 1 and 2 express the same quantity and, thus:

$$\frac{dP_{CO_2(t)}^{bubble}}{dt} = -k_L a_B RT \left( \frac{P_{CO_2(t)}^{bubble}}{h} - [dCO_2]_{(t)} \right), \tag{3}$$

where  $a_B = S_B/V_B$ .

The dynamics of the CO<sub>2</sub> partial pressure in a bubble can be calculated analytically assuming that the liquid volume is much larger than the bubble volume  $V_L \gg V_B$  and, thus, the mass transfer from the single bubble changes the concentration of the dissolved CO<sub>2</sub> negligibly:

$$\frac{d}{dt} \left( \frac{P_{CO_2(t)}^{bubble}}{h} \right) \gg \frac{d}{dt} [dCO_2]_{(t)}, \text{ i.e., } [dCO_2] \text{ is approximately}$$

constant during the lifetime of a bubble. Then, Eq. 3 can be approximated by

$$h \frac{d}{dt} \left( \frac{P_{\text{CO}_2(t)}^{\text{bubble}}}{h} - [\text{dCO}_2] \right) = -k_L a_B RT \left( \frac{P_{\text{CO}_2(t)}^{\text{bubble}}}{h} - [\text{dCO}_2] \right). \quad (4)$$

Using the initial condition  $P_{\text{CO}_2(t=0,s)}^{\text{bubble}} = P_{\text{CO}_2}^{\text{IN}}$ , Eq. 4 can be solved to:

$$P_{\text{CO}_2(t)}^{\text{bubble}} = P_{\text{CO}_2}^{\text{IN}} \left[ \exp \left( - \left( \frac{k_L a_B RT}{h} t \right) \right) \right] + h [\text{dCO}_2] \left[ 1 - \exp \left( - \left( \frac{k_L a_B RT}{h} t \right) \right) \right]. \quad (5)$$

Extending the calculation to a flow of  $N_B$  bubbles, Eq. 6 can be derived to quantify the mass transfer rate from the bubble flow to the liquid phase ( $\alpha_{\text{CO}_2}$  in Fig. 1):

$$\alpha_{\text{CO}_2} = N_B \frac{\Delta n_{\text{CO}_2}}{\tau} = N_B \frac{V_B}{RT} \frac{P_{\text{CO}_2}^{\text{IN}} - P_{\text{CO}_2}^{\text{X}}}{\tau} = \frac{J}{RT} (P_{\text{CO}_2}^{\text{IN}} - P_{\text{CO}_2}^{\text{X}}), \quad (6)$$

where  $P_{\text{CO}_2}^{\text{X}} = P_{\text{CO}_2(t=\tau)}^{\text{bubble}}$  is the  $\text{CO}_2$  partial pressure of the gas entering the headspace from the bubble flow (Fig. 1), which can be calculated from Eq. 5 to yield

$$\alpha_{\text{CO}_2} = \frac{J}{RT} \left\{ P_{\text{CO}_2}^{\text{IN}} - h [\text{dCO}_2]_{(t)} \right\} \left\{ 1 - \exp \left[ - \left( \frac{k_L a_B RT}{h} \tau \right) \right] \right\}. \quad (7)$$

The bubble stream brings into the headspace a flux of gas  $J$  of  $\text{CO}_2$  partial pressure  $P_{\text{CO}_2}^{\text{X}} = P_{\text{CO}_2(t=\tau)}^{\text{bubble}}$  that can also be calculated from Eq. 5. The corresponding mass transfer flux (Fig. 1) is

$$B(t) = \frac{J}{RT} \left\{ P_{\text{CO}_2}^{\text{IN}} \exp \left( - \left( \frac{k_L a_B RT}{h} \tau \right) \right) + h [\text{dCO}_2]_{(t)} \left[ 1 - \exp \left( - \left( \frac{k_L a_B RT}{h} \tau \right) \right) \right] \right\}. \quad (8)$$

Another  $\text{CO}_2$  mass transfer processes occur across the photobioreactor water surface from the headspace:

$$\beta(t) = -k_L S_H \left( \frac{P_{\text{CO}_2(t)}^{\text{OUT}}}{h} - [\text{dCO}_2]_{(t)} \right), \quad (9)$$

and due to the gas leaving the headspace through the exhaust:

$$\Gamma(t) = - \frac{J}{RT} P_{\text{CO}_2(t)}^{\text{OUT}}. \quad (10)$$

The  $\text{CO}_2$  partial pressure in the headspace and, thus, in the outgoing gas is determined by sum of the fluxes in and out of the headspace:

$$\frac{dP_{\text{CO}_2(t)}^{\text{OUT}}}{dt} = \frac{RT}{V_H} [B(t) + \beta(t) + \Gamma(t)], \quad (11)$$

where  $V_H$  is the volume of the headspace. Equation 11 can be integrated numerically to reveal the dynamics of the  $\text{CO}_2$  partial pressure in the headspace.

The  $\text{CO}_2$  mass transfer processes of rate  $\alpha_{\text{CO}_2}$  from the bubble flow and  $\beta_{\text{CO}_2}$  from the headspace modify the concentration of the carbon dioxide dissolved in the liquid phase  $[\text{dCO}_2]$ :

$$\frac{d[\text{dCO}_2]}{dt} = \frac{J}{RT V_L} h \left( \frac{P_{\text{CO}_2}^{\text{IN}}}{h} - [\text{dCO}_2]_{(t)} \right) \times \left\{ 1 - \exp \left[ - \left( \frac{k_L a_B RT}{h} \tau \right) \right] \right\} - k_L \frac{S_H}{V_L} \left( \frac{P_{\text{CO}_2(t)}^{\text{OUT}}}{h} - [\text{dCO}_2]_{(t)} \right). \quad (12)$$

Using  $P_{\text{CO}_2(t)}^{\text{OUT}}$  from the numerical integration of Eq. 11, Eq. 12 can also be integrated numerically to yield the dynamics of the dissolved  $\text{CO}_2$   $[\text{dCO}_2]$  at low pH (negligible reaction to bicarbonate) and in the absence of algae.

At neutral pH, the dissolved  $\text{CO}_2$  can be hydrated to bicarbonate (Fig. 1). The alternative pathway involving carbonic acid (dashed arrows in Fig. 1) is integrated in form of effective rates of  $\text{CO}_2$  hydration  $k$  and of  $\text{HCO}_3^-$  dehydration  $l$  as in [24]. The reactions involving bicarbonate are included in Eqs. 13 and 14:

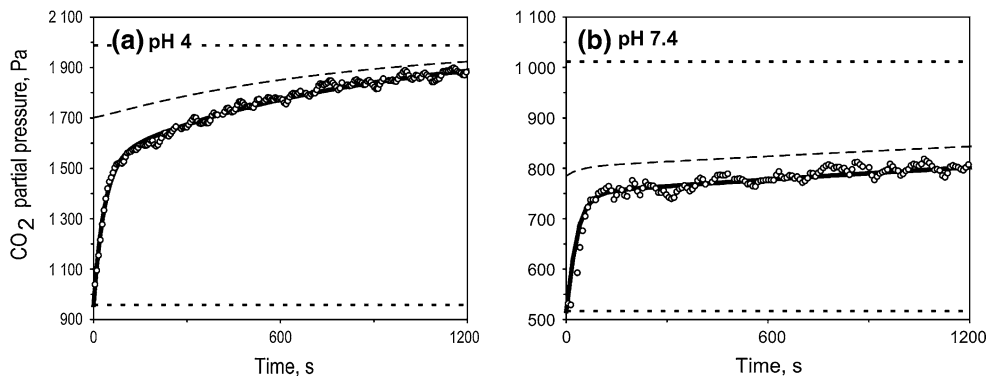
$$\frac{d[\text{dCO}_2]_{(t)}}{dt} = \frac{J}{RT V_L} h \left( \frac{P_{\text{CO}_2}^{\text{IN}}}{h} - [\text{dCO}_2]_{(t)} \right) \times \left\{ 1 - \exp \left[ - \left( \frac{k_L a_B RT}{h} \tau \right) \right] \right\} - k_L \frac{S_H}{V_L} \left( \frac{P_{\text{CO}_2(t)}^{\text{OUT}}}{h} - [\text{dCO}_2]_{(t)} \right) + \ell [\text{HCO}_3^-]_{(t)} - k [\text{dCO}_2]_{(t)} - \gamma_{\text{dCO}_2}, \quad (13)$$

$$\frac{d[\text{HCO}_3^-]_{(t)}}{dt} = k [\text{dCO}_2]_{(t)} - \ell [\text{HCO}_3^-]_{(t)} - \gamma_{\text{HCO}_3^-}. \quad (14)$$

The rates  $\gamma_{\text{dCO}_2}$  and  $\gamma_{\text{HCO}_3^-}$  represent the uptake of dissolved carbon dioxide  $\text{dCO}_2$  and of bicarbonate  $\text{HCO}_3^-$  by algae as well as the cycling between these forms [7, 9, 19].

## Technical experiment

The dynamics of the  $\text{CO}_2$  partial pressure in the exhaust of the bioreactor was measured during a transition caused by an abrupt change of the  $\text{CO}_2$  partial pressure at the photobioreactor gas input (open circles in Fig. 2). The same dynamics were modeled as described above using Eq. 11 (thick solid lines in Fig. 2).



**Fig. 2** Modeled and measured CO<sub>2</sub> partial pressure in the photobioreactor exhaust gas under different conditions. **a** pH 4.0,  $T = 303$  K, at  $t = 0$  s equilibrium with  $P_{\text{CO}_2}^{\text{IN}} = 946$  Pa and  $t > 0$  s  $P_{\text{CO}_2}^{\text{IN}} = 1962$  Pa. **b** pH 7.4,  $T = 303$  K, at  $t = 0$  s equilibrium with  $P_{\text{CO}_2}^{\text{IN}} = 510$  Pa and  $t > 0$  s  $P_{\text{CO}_2}^{\text{IN}} = 998$  Pa. Dotted lines indicate the starting ( $t \leq 0$  s) and set ( $t \geq 0$  s) CO<sub>2</sub> partial pressure at the input of the

photobioreactor. Open circles show the measured CO<sub>2</sub> partial pressure in the photobioreactor exhaust, and thick solid lines under the circles show the model prediction. The dashed line shows the modeled CO<sub>2</sub> partial pressure in the bubbles at the time when they reach the water surface

The fixed parameters were: photobioreactor liquid volume  $V_L = 1.2 \times 10^{-3}$  m<sup>3</sup> (1.2 l), liquid to headspace surface  $S_H = 6.3 \times 10^{-3}$  m<sup>2</sup>, gas flow rate  $3.3 \times 10^{-6}$  m<sup>3</sup> s<sup>-1</sup> (200 ml min<sup>-1</sup>), and mean number of bubbles  $N_B \approx 400$  (counted from photographs). The bubble lifetime, the headspace volume, and the mass transfer coefficient were considered variable and found by using the Solver add-on to the Excel program (Microsoft Corp., USA) for the best fit between the data and the model.

The bubble lifetime was  $\tau \approx 1.2$  s, and the mean bubble radius was  $r_B \approx 1.3 \times 10^{-3}$  m. The headspace volume was  $V_H \approx 158 \times 10^{-6}$  m<sup>3</sup> (158 ml) in the experiment with pH 4.0, and  $172 \times 10^{-6}$  m<sup>3</sup> (172 ml) with pH 7.4. The difference in head volumes is explained by evaporation of media during lengthy repetitions of the experiments.

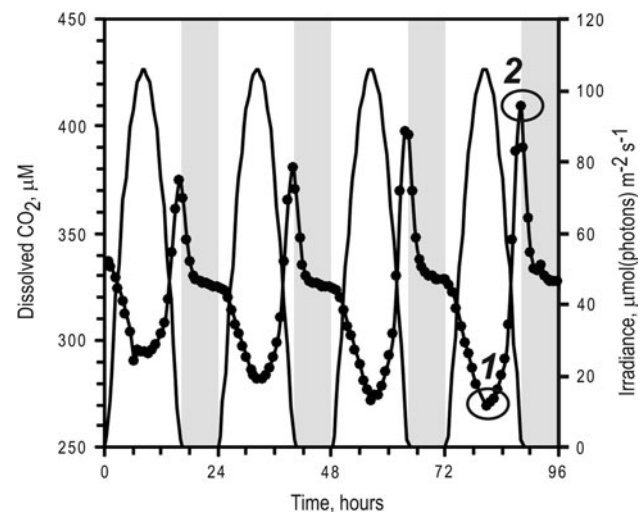
The numerical fit for the mass transfer yielded a coefficient value of  $k_L \approx 1.36 \times 10^{-4}$  m s<sup>-1</sup> in the experiment with pH 4.0, and  $1.78 \times 10^{-4}$  m s<sup>-1</sup> with pH 7.4.

Other fitted parameters in pH 7.4 were the effective rate constants of CO<sub>2</sub> hydration ( $k \approx 2.1 \times 10^{-2}$  s<sup>-1</sup>) and of HCO<sub>3</sub><sup>-</sup> dehydration ( $l \approx 2.2 \times 10^{-3}$  s<sup>-1</sup>). The model predictions also matched dynamics of dissolved CO<sub>2</sub> (not shown).

### Modeling a biological experiment

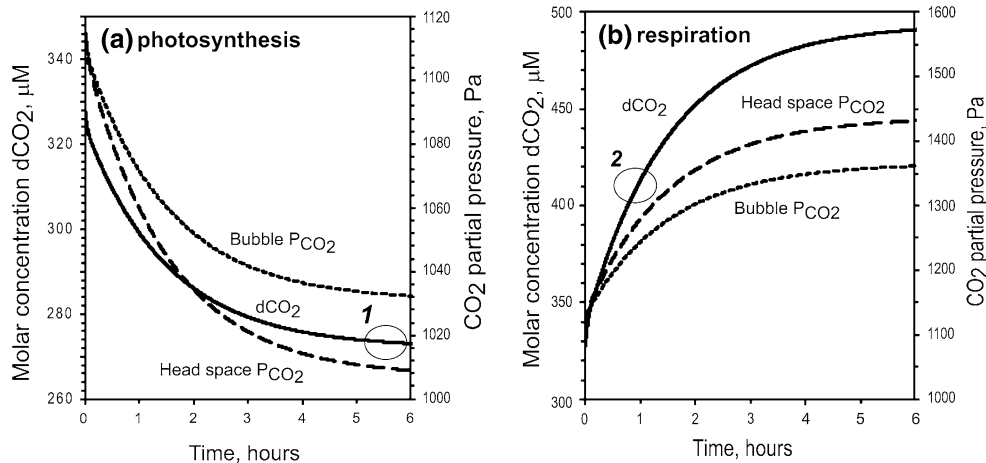
The dynamics of the CO<sub>2</sub> distribution in algal photobioreactors is massively influenced by the metabolic activities. Figure 3 shows the dynamics of dissolved CO<sub>2</sub> (full circles) in a photobioreactor [2, 15] in which a culture of *Cyanothece* sp. ATCC 51142 was grown in 16 h light (solid line) and 8 h dark (grey columns). A homologous experiment was comprehensively described previously [3].

Upon illumination in the morning, the cyanobacteria lower the dissolved CO<sub>2</sub> concentration approximately in



**Fig. 3** Concentration of dissolved CO<sub>2</sub> (closed circles) in a photobioreactor described in Ref. [15]. The diurnal modulation of dissolved CO<sub>2</sub> was caused by intense metabolic activity of the cyanobacterium *Cyanothece* sp. ATCC 51142 grown in the photobioreactor. Temperature was 30°C, pH was stabilized at 7.5, and the flow of CO<sub>2</sub>-enriched air was 200 ml min<sup>-1</sup>. The CO<sub>2</sub> concentration at the photobioreactor input was 11,000 ppm (~1,115 Pa). Other details of the experimental materials and methods were as in Ref. [3]

proportion to the incident irradiance. The maximum depression was reached in the early afternoon hours to ~270 μM dCO<sub>2</sub> (labeled 1 in Fig. 3). This is where the maximal combined photosynthetic and Ci cycling rate are reached in the culture. Later in the afternoon, the metabolic transition from fast photosynthesis and Ci cycling to strong respiration [3] and CO<sub>2</sub> release from the internal pool was manifested by the sharp increase of dCO<sub>2</sub> well above equilibrium to ~410 μM dCO<sub>2</sub> (labeled 2 in Fig. 3). The prevailing respiration can be modeled by negative values of the rate  $\gamma_{\text{dCO}_2}$  in Eq. 13. The dusk respiratory peak is very



**Fig. 4** Dynamics of dissolved  $\text{CO}_2$  (solid line) calculated for cyanobacterial photosynthetic activity (a) of  $70 \times 10^{-3} \text{ mol}(\text{CO}_2) \text{ mol}(\text{Chl})^{-1} \text{ s}^{-1}$  at culture density of  $1.7 \mu\text{M}(\text{Chl})$ . The model parameters were as described above. The input partial pressure of  $\text{CO}_2$  was as in Fig. 3 ( $\sim 1,115 \text{ Pa}$ ). Photosynthetic activity was

dynamic—its typical half-time period can be estimated by Fourier analysis of the transient at around 3.25 h, while the amplitude of the respective modulation was  $\sim 70 \mu\text{M dCO}_2$ .

Figure 4 documents that, solving numerically our model equations 13 and 14, one can show that cyanobacterial suspension corresponding to pigment density of  $1.7 \times 10^{-6} \text{ M}(\text{Chl})$  of typical photosynthetic and  $\text{C}_i$  cycling activity of  $70 \times 10^{-3} \text{ mol}(\text{CO}_2) \text{ mol}(\text{Chl})^{-1} \text{ s}^{-1}$  [2, 10] can lower the dissolved  $\text{CO}_2$  to  $\sim 270 \mu\text{M dCO}_2$  (labeled 1 in Figs. 3 and 4a). The transition due to the gradually increasing photosynthetic  $\text{CO}_2$  uptake (depression around midday in Fig. 3) is relatively slow and, thus, is not significantly limited by the  $\text{CO}_2$  mass transfer between the gas and water in the photobioreactor. The sharp respiratory peak in the late afternoon hours is a dynamic feature that cannot be accounted for by a steady state. Figure 4b shows an attempt to model respiratory activity that could lead to a rapid ( $\sim 1 \text{ h}$ ) increase to  $410 \mu\text{M dCO}_2$  (labeled 2 in Fig. 3). The respiration activity leading to this result was  $\sim 3$  times higher than the photosynthetic activity estimated in Fig. 4a to elicit a sharp rise similar to that in Fig. 3 (label 2).

The capacity of the model to provide insights that would be difficult to measure experimentally is demonstrated by the calculated dynamics of the  $\text{CO}_2$  partial pressure in the bubbles reaching the water surface (dotted lines in Fig. 4a, b). In contrast, the  $\text{CO}_2$  partial pressure in the headspace (dashed lines in Fig. 4a, b) can be directly measured and used for future model validation.

## Conclusions

The model presented herein offers insight into the dynamics of fluxes of different forms of  $\text{CO}_2$  in an algal

modeled as starting at  $t = 0 \text{ h}$ . **b** Modeled effect of respiratory activity that was supposed to be 3 times higher than the photosynthetic activity in **a**. The dotted and dashed lines in both **a** and **b** show the calculated partial pressure of  $\text{CO}_2$  in bubbles reaching the water surface and in the headspace, respectively

photobioreactor. The model fits experimental data measured during a transition between different levels of input partial pressure of  $\text{CO}_2$  at pH 4.0 and pH 7.4. The fit was obtained with variable rate constants of  $\text{dCO}_2$  hydration ( $k$ ) and  $\text{HCO}_3^-$  dehydration ( $l$ ). The best fit was obtained for  $k \approx 2.1 \times 10^{-2} \text{ s}^{-1}$  and  $l \approx 2.2 \times 10^{-3} \text{ s}^{-1}$ . These values are not far from earlier reported values [24] for pH 7.5 ( $k \approx 4.0 \times 10^{-2} \text{ s}^{-1}$  and  $l \approx 3.5 \times 10^{-3} \text{ s}^{-1}$ ).

The model was further validated by explaining the midday depression in dissolved  $\text{CO}_2$  concentration due to photosynthetic activity of cyanobacteria that agrees with typically measured rates. The most important conclusion of the paper is that the dissolved  $\text{CO}_2$  and bicarbonate concentrations in the photobioreactor media can be displaced far from equilibrium by metabolic events, such as the dynamic respiratory peak of *Cyanotheca* sp. that occurs in late afternoon hours of the diurnal cycle. Such dynamic events can dramatically affect the carbon balance of algal bioreactors in industrial applications. Also affected will be the energetic content of the produced biomass.

Model approximations and an outlook on further model improvement

Further refinement of the model is planned to account for diverse pH regimes. Namely, one may wish to model the frequent bioreactor regimes in which the suspension pH is automatically adjusted by bursts of  $\text{CO}_2$  or with free-drifting pH, experimental modes described in detail previously [15, Figs. 6B or Fig. 6A]. Issues that should also be considered are real-life deviations from the present model assumptions. Namely, we assumed that diverse bubbles in the modeled photobioreactor volume can be represented by

a uniform and constant effective size of bubbles with identical lifetime. In real flat-panel photobioreactors a uniform bubble lifetime is hard to achieve because of the statistical bubble radius dispersion and frequently uneven flow rates of bubbles along the horizontal photobioreactor profile. Also, we neglected the fact that the pressure in bubbles leaving the sparger tube is higher than in bubbles approaching the water surface. The effect on the bubble size of the CO<sub>2</sub> transfer during the bubble lifetime is on the other hand tiny, as the typical CO<sub>2</sub> concentrations are from 380 ppm to 20,000 ppm. Furthermore, the partial removal of CO<sub>2</sub> from the bubbles is compensated by O<sub>2</sub> uptake during the day, and vice versa at night. Among the issues that remain to be addressed are effects of salinity and ionic strength in the media [28, 31]. For that, integration with existing models [14, 22] will be pursued.

In spite of these limitations, we expect that the proposed improvements will be formulated as amendments of the model proposed here rather than its replacement.

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